

To D. R. DeLaporte Date June 5, 1963.  
From E. O. Foster Ref. \_\_\_\_\_  
Subject Correspondence to MKP dated 24 May, 1963 from J. P. Windish

This is offered as an explanation of the major discrepancies identified as Items 11 and 38 in the correspondence.

The primary object of the plant flow sheet was to identify the sources of soluble arsenic in our Treatment Plant, to follow the course of the solutions through the circuits, and to show the locations where arsenic bearing solutions are disposed of.

Through the extraction circuits where dissolution of arsenic occurs, determinations for arsenic were made by chemical analysis for both solutions and solids.

In the "sand preparation" circuit, where the major discrepancies occurred, only the solutions were assayed, and the arsenic content for solids was calculated by difference. The assays reported for sand plant solids were calculated incorrectly.

Re: Table 4 of Mr. Windish's letter - We should explain it is possible to have a weight loss during roasting, varying from 18 to 23 per cent. An increase in weight occurs by oxidation of the distilled arsenic to  $As_2O_3$ . This accounts for the difference of 7 tons in the solids weights. The 90 tons of water missing enters the roaster as part of the slurry feed and is vaporized as Mr. Windish anticipated.

Page 2 - The figures in red ink were not corrections, but revisions due to improvements in Cottrell operation, ex-insulating hoppers and increasing temperature to produce clean dust.

Page 2 Re: Precipitated Arsenic

Arsenic precipitation as insoluble ferric arsenite occurs in the final tailings and is discharged as a suspended solid with tailings and is impounded in Bow Lake.

A corrected flow sheet for Sand Preparation is attached.